

Advances in Shell Room with quick setting polymer additive for ceramic back up slurries

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Abstract

REMET has formulated the industry's first quick setting polymer which confers the advantage of fast drying whilst maintaining reliable and convenient slurry characteristics and maintenance. In order to quantify the performance and operating mechanism of the polymer, a series of experiments have been carried out to compare the new formulation with one of REMET's most popular traditional enhancement polymers. Measurement of the modulus of a the new enhanced slurry and a traditional slurry by DMA during drying has enabled the gelation points of each system to be accurately determined. Measurement of temperature drop during drying has been used to compare the facility of water evaporation from the quick drying slurry and traditional slurry under identical conditions. The results confirm that not only is the quick drying polymer system faster to gel, but that the rate of water evaporation is unimpeded by the gelation process.

O'Fallon Casting is using this polymer and a colloidal silica binder in an experimental capacity for the replacement of an ethyl silicate slurry system. The application of ammonia vapors to an ethyl silicate shell layer induces a quick gelling of the binder, offering control of the drying process. Traditional polymer systems have failed to support the conversion to a colloidal silica binder while preserving the low viscosity range achievable with ethyl silicate. New formulations using the novel polymer concentrate have performed

successfully in achieving two principle qualities of an alcohol slurry system: a rapid gelling time, and a reduced cold strength for ease of knockout. A case study is presented here to demonstrate the development of a trial slurry recipe at O'Fallon Casting using the quick drying polymer, and the iterative progression of the formula through MOR testing and the reduction of shell-related casting defects.

Introduction

With increasing demands on the Investment Casting industries to reduce lead time by novel technologies including Additive Manufacturing, there have been many attempts to reduce the lead time through the shell room. These have been met with limited success and are summarized below.

Remet set out to product a novel material which would reduce lead times while maintaining or improving the strength of the shell system. QUIKSET™, a novel polymer concentration was introduced and tested.

Background

Polymer science has gone from strength to strength since the introduction of polymers to shell systems. The addition of the polymer affects the green strength of the shell during drying and autoclave de-wax while also improving dry time. Following burnout, the polymer is no longer present which creates voids, weakening the shell to allow for easier knockout. While cooled, the shell exhibits similar strengths to a shell system with no polymer, allowing for easy shell removal. This can be seen within figure 1 below.

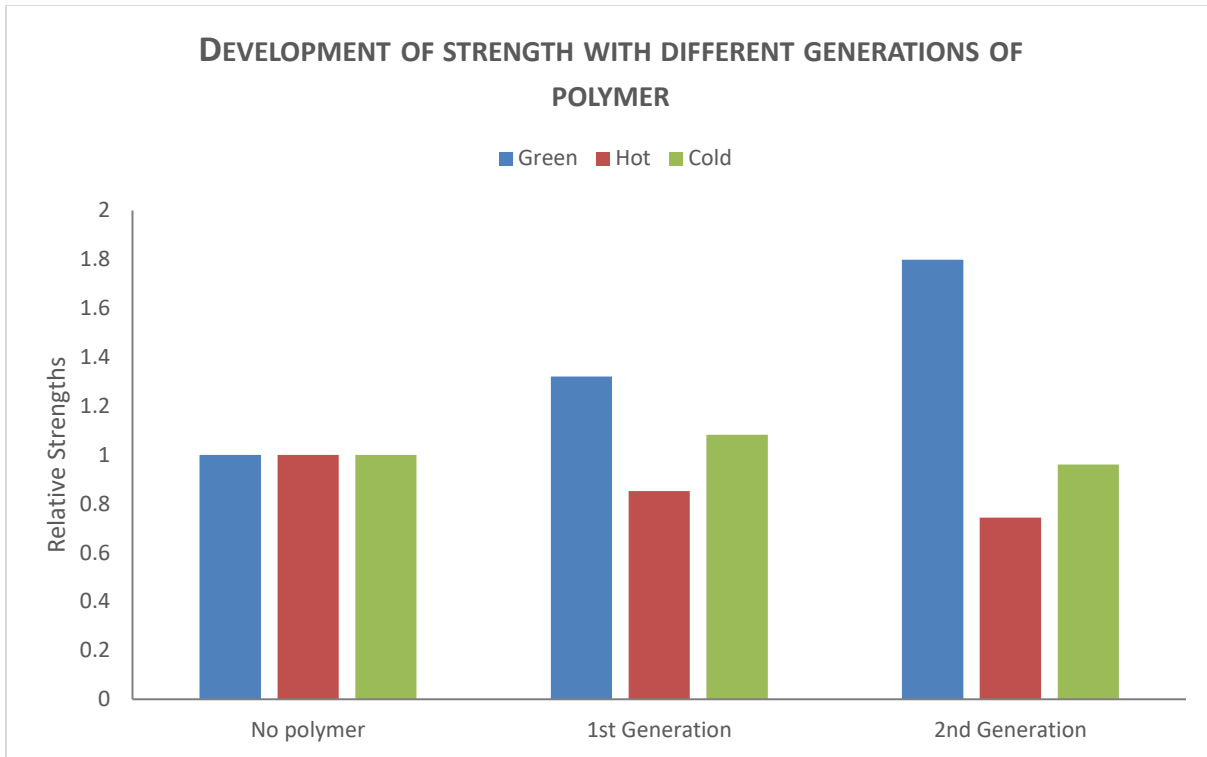


Figure 1 Development of strength with different generations of polymer

With this increase in strength, issues of BoilerClave cracking and drying defects are greatly reduced. However, the drying times are still quite long and delay processing of components within the process. Within this paper we will present AdBond® Quickset™ polymer concentrate technology which greatly reduces dry time without the need for infrastructure or modified dipping programs.

Fundamentals of drying

There are two ways of drying a colloidal silica sol, one is through the change in pH toward pH 7 as indicated in Figure 2.

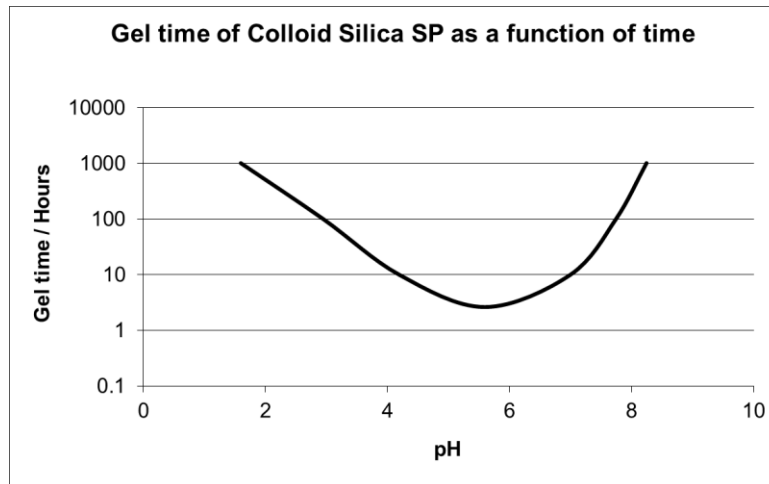


Figure 2 Gel time as a function of pH

The second mechanism is through the removal of the water, which brings the silica particles together to gel the sol and create a solid matrix. This solid matrix then stiffens and creates bonding of the ceramic.

Within a shell system, it is difficult altering the pH, as the slurry life will shorten and cause instabilities within the process. Increasing the water removal rate has been attempted through many methods. These include:

1. **Rapid Air Drying** – High speed air drying system technology have been introduced to increase the water removal rates [1]. The infrared technology utilizes rapid removal of water while counteracting the temperature drop of the wax by infrared light to maintain dimensional stability.
2. **Microwave drying** - Microwave drying has been utilized to remove water from the shell [2]. This system allows reports it can control drying conditions to affect the mechanical properties of the shell.
3. **Rapid Shell Drying** – Rapid Shell Drying has utilized the use of Super Absorbent Polymers to reduce drying times by pulling the water from the sol and storing it within

the absorbent polymer. There are drawbacks to this method, including a reduction in strength of the ceramic [3].

4. **Desiccant based systems** – These systems used a silica gel to remove water from the shell system and into the stucco layer [4]. Again, the drawback of these methods is the retention of water within the shell during drying.

Within items 1 & 2 mentioned above, significant capital investment is required. These can be unfeasible for many foundries. For items 3&4 the retention of water within the shell can reduce the strength of the shell and be susceptible to cracking and bulging during firing.

Remet has formulated an innovative AdBond® QUIKSET™(QS) technology to accelerate removal of water from the shell to ensure no water is trapped within the matrix during re-dipping. Using a proprietary polymer combination, it allows for the gelation of the slurry but also keeps a path free for water to travel to the surface of the mould and be removed during drying. This can be seen visually within Figure 3 Simplified gelation of slurry within a shell system.

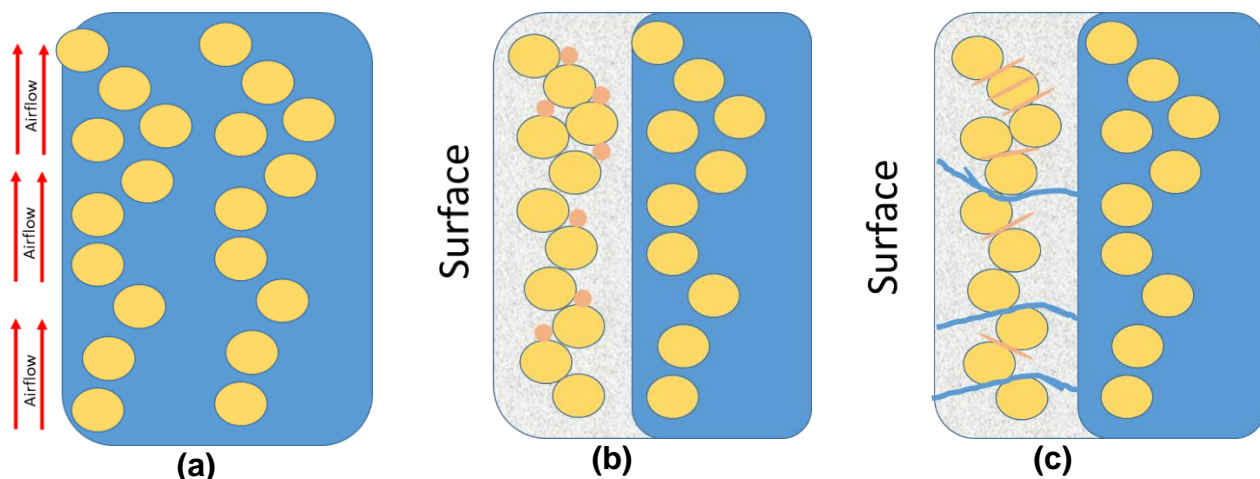


Figure 3 Simplified gelation of slurry within a shell system (a) ungelled slurry (b) gelation of traditional polymer shells (c) Gelation of QuikSet Slurry

Materials and Methods

Slurry Formulation

The formulations below were utilized for the slurries under review.

Table 1 Slurry formulation for mechanical testing

Component:	Ultra	QuikSet
Fused Silica 200 Mesh	62.92%	60.87%
SP-30	31.46%	30.43%
Polymer	4.5% Ultra	7.60% QuikSet
Wetin	0.90%	0.87%
Burst 100	0.22%	0.22%

9 back up layers and a seal coat was applied to the shell at one hour inter-coat dry time.

The below formulations were used for the DMA and thermal analysis testing can be found within table 2.

Table 2 Slurry formulation for DMA and thermal analysis

Component:	AdBond Advantage	QuikSet
Zircon 200	62 %	62%
Binder	32.00%	30.40% SP 30
Polymer	6%	7.60%

Mechanical Analysis

Flexural testing is used to ascertain the flexural strength of the shell systems. The strength of the ceramic shells is a measure of the resistance to failure through the investment casting process. Many external stresses are experienced by the shell during de-wax, preheat, metal pour and solidification. The ability to resist fracture through these processes is vital to a successful shell system.

Testing was carried out in accordance with BS 1902: Part 4: section 4.4:1984 [5] . 20 x 80 mm samples were tested on a Lloyd xxx. Flexural testing was carried in the testing setup shown in Figure 3.

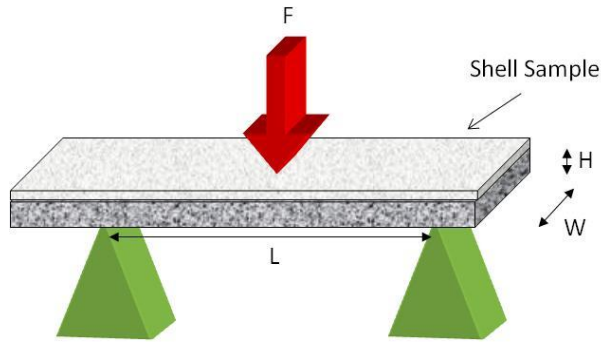


Figure 4 3-point schematic

Samples were tested green, hot (1000 °C) and fired and cooled. A load application rate of 1 mm min⁻¹ was used for all bend testing. The bend failure strength $\sigma_{Flexural}$ was calculated using Equation 1.

$$\sigma_{3_Point_Flexural} = \frac{3P_{MAX}L}{2WH^2}$$

Equation 1

where P_{MAX} is the fracture load, L , W and H are the length, width and thickness of sample fracture area respectively.

Permeability is an important property of an investment casting shell system. The permeability of a shell allows air to escape from the mould during casting, thus reducing back pressure and the likelihood of non-fill during casting. It can also reduce the chances of shell cracking under internal pressure. High permeability also assists during the shell removal stage. Permeability measurements give an assessment of the level of connected porosity in the shell. This may also be an indicator of shell strength.

Tests were performed in accordance with BS 1902: Section 10.2:1994. Test pieces were made using “International Table Tennis Federation (ITTF) approved 3 star table tennis balls and impervious mullite ($\text{Si}_4\text{Al}_6\text{O}_{13}$) rods” at a temperature of 1000°C [6].

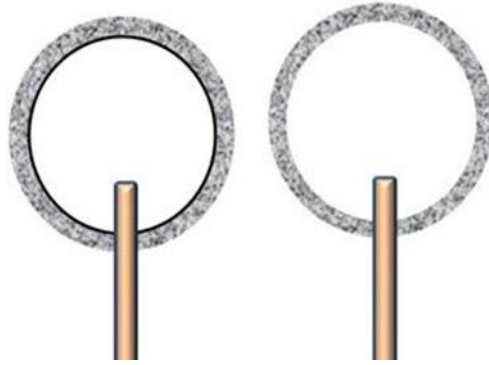


Figure 5 Permeability Sample with and without ping pong ball

Permeability measurements were taken at time intervals up to one hour to assess the effect of sintering on the samples analysed. Equation 2 was used to determine the permeability of the samples:

$$\mu = \frac{sV_c\eta}{a\Delta P} \quad \text{Equation 2}$$

where μ is the permeability, s is the wall thickness of the sample, V_c is the volumetric flow rate, η is the dynamic viscosity of air at the elevated temperature, a is the inner surface area of the tennis ball and ΔP is the pressure difference.

Dynamic Mechanical Analysis

Dynamic Mechanical Analysis (DMA) is a mechanical method of analyzing material properties while under a dynamic response. This cutting edge testing can analyse the expansion and contraction of waxes, the dynamic loading of a wax at different temperatures, and also the gelation of slurry.

A defined volume of slurry was thinly coated on a rubber sample, this sample was then oscillated at a constant deflection to assess the force required to stress the sample. A control sample of slurry was compared to the new QuikSet™ slurry at constant temperature and humidity settings.

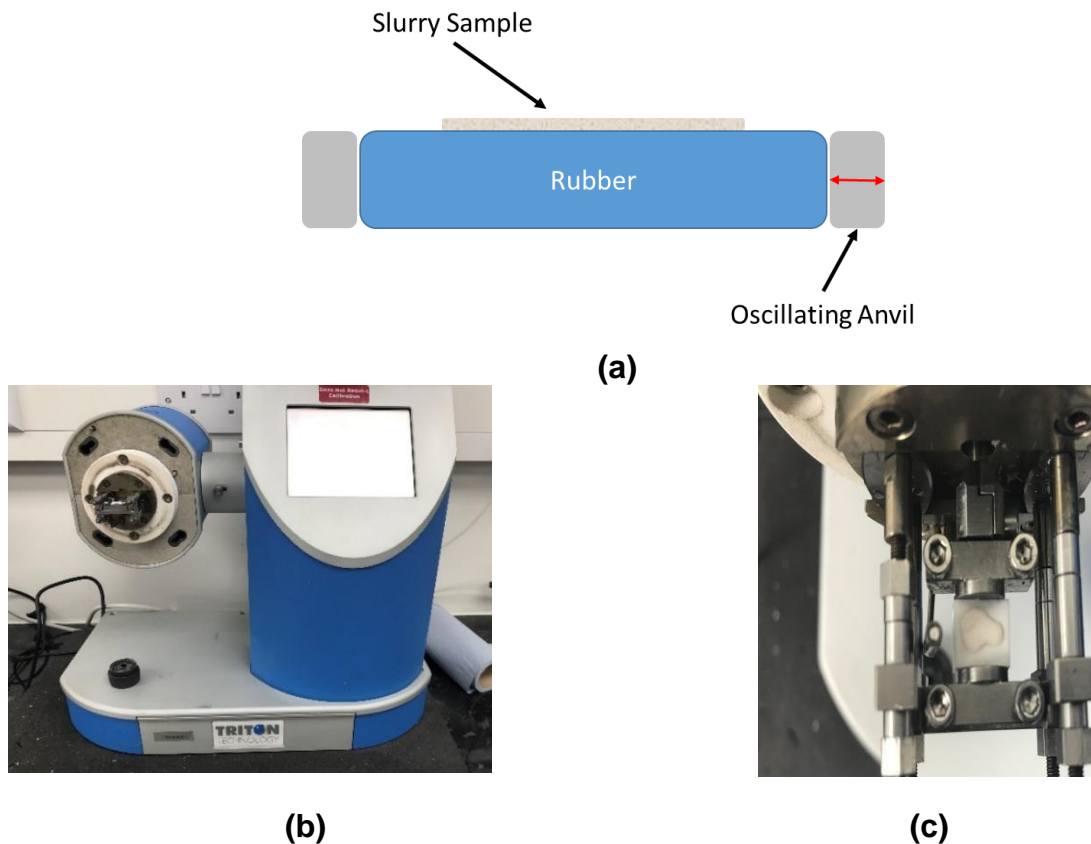


Figure 6 DMA Setup to assess gelation of slurries. (a) Testing Schematic (b) Test Rig (c) Samples within sample holder

Infrared Image Analysis

The temperature difference between the two slurries was also calculated using thermal imaging. Samples of the same volume were placed in a defined wax substrate to mimic drying on a wax pattern. The samples were placed in a controlled temperature and humidity environment with low air flow rate.

A video was captured using a micro epsilon thermo imager and a single point on each sample was logged for temperature over time. This data was then inputted into excel to give a relationship of temperature over time.

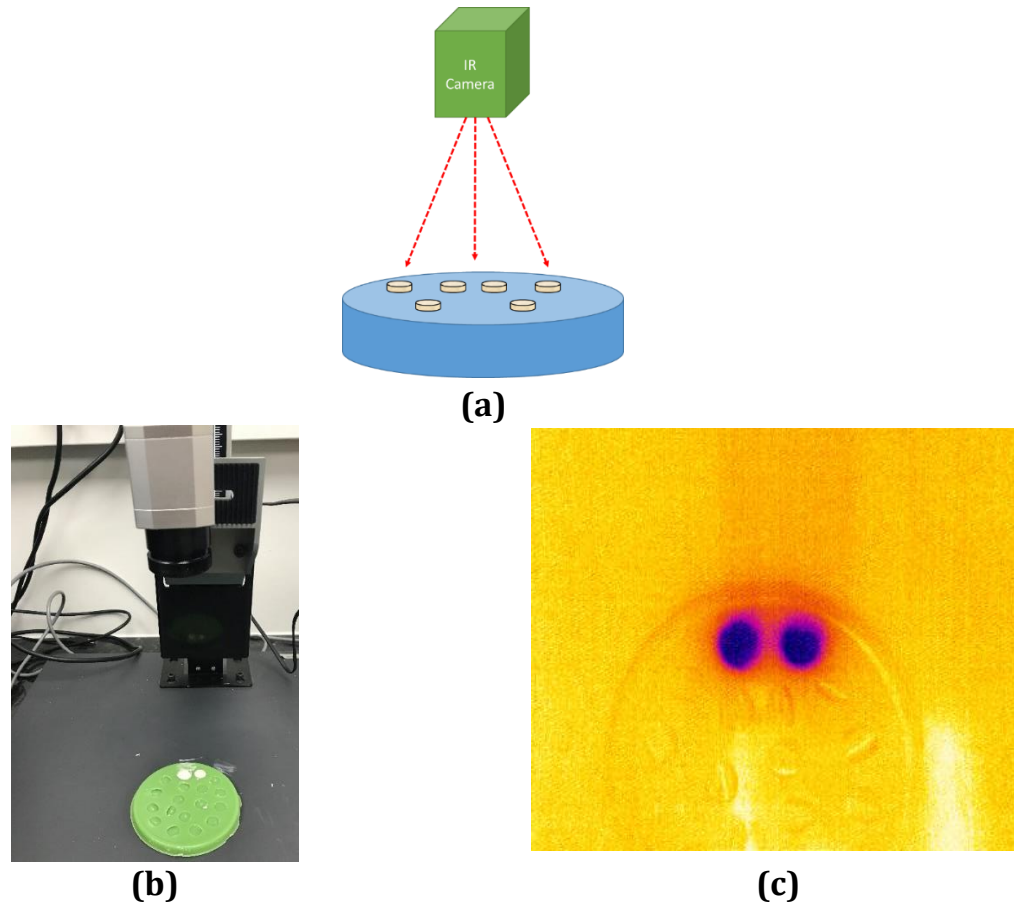


Figure 7 Thermal imaging camera setup (a) Testing schematic (b) Test setup (c) IR image captured of the slurries drying

Results & Discussion

Mechanical Analysis

The flexural strength results for the samples can be found within Figure 8.

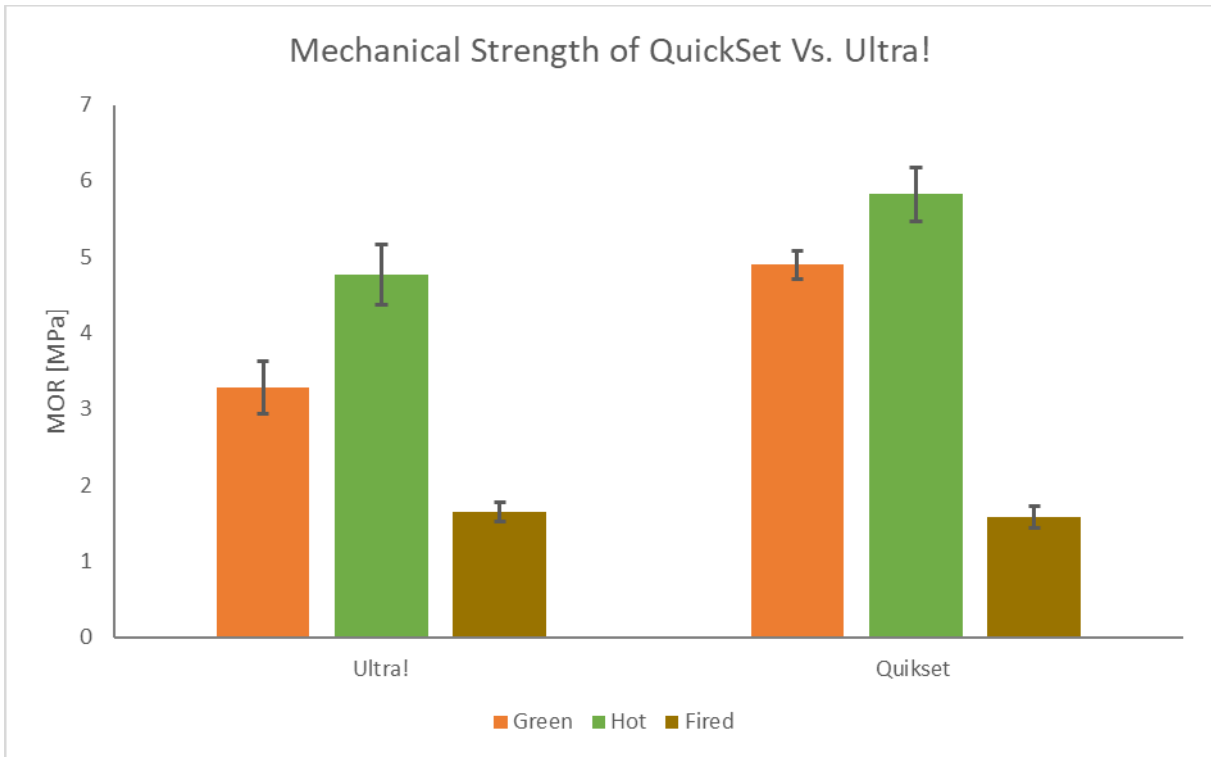


Figure 8 Flexural Strength (MOR) of Ultra vs. QuikSet slurries [N=4]

The permeability results can be found in Figure 9.

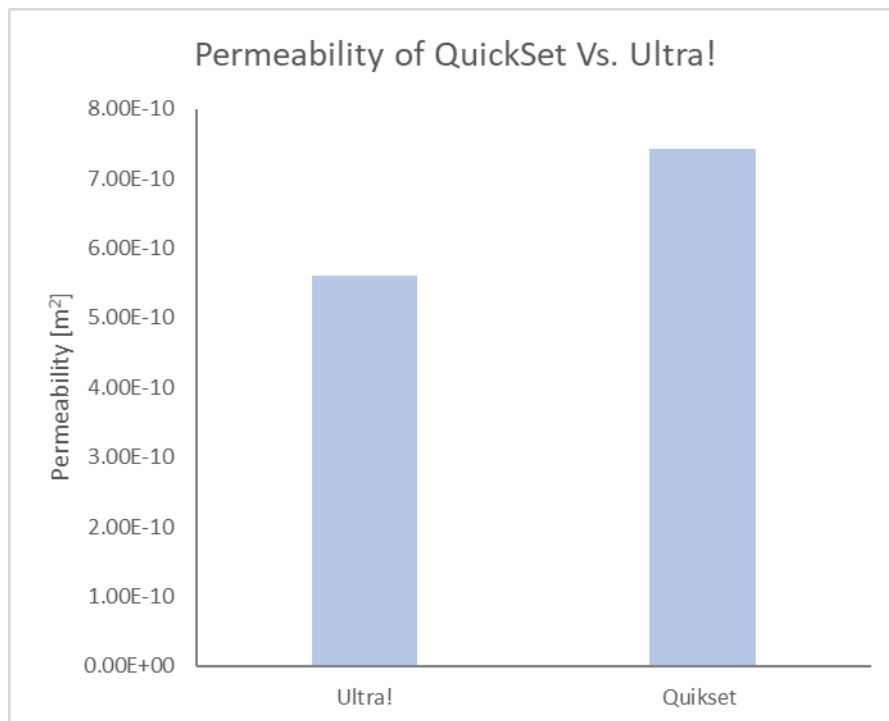


Figure 9 Permeability of Ultra Vs. QuikSet materials using the ping pong method [n=3]

The mechanical testing shows the strength of the QuickSet slurry is 49 % stronger in the green strength with a 22 % increase while hot. This increase in strength then drops to comparable values when fired and cooled, allowing for easy knock out.

Even with this increase in strength, there is also an increase in permeability by 46 %. This is due to a high polymer content within the system opening voids and improving air flow through the shell.

Thermal Analysis

The thermal imaging has the ability to show the recovery of the shell during drying. The thermal imaging camera was configured to give a temperature readout from the middle of the sample. Figure 10 shows the temperature over time.

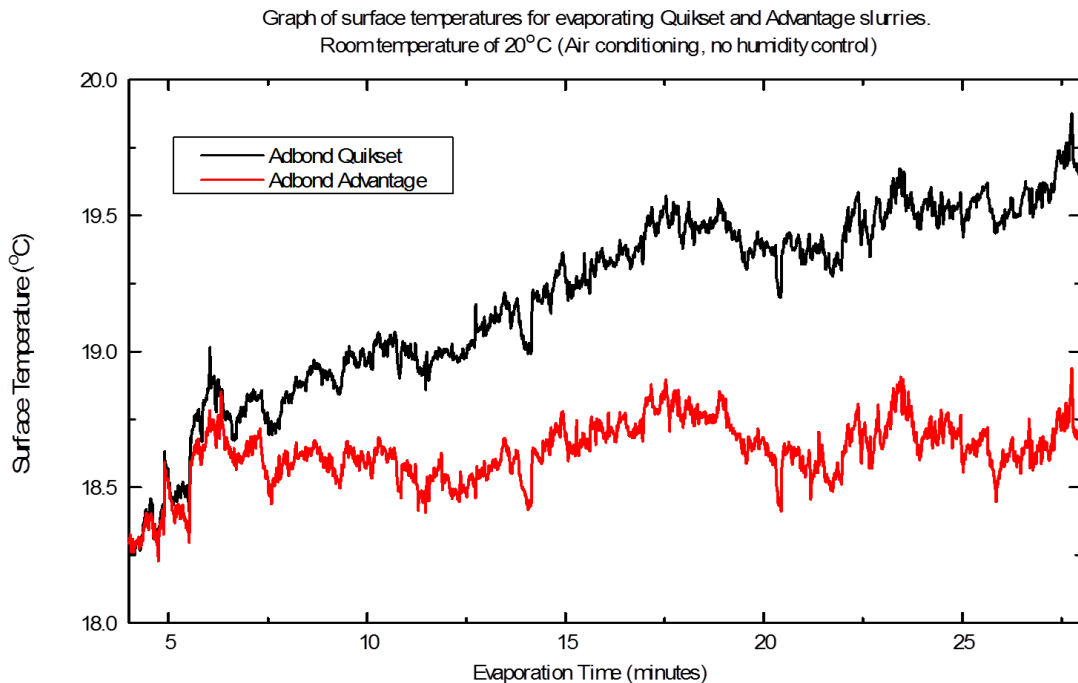


Figure 10 Plot of temperature of QS and AdBond Advantage slurry over time during drying

As can be seen within this graph, the QS slurry has recovered temperature much quicker than the traditional slurry. After 30 minutes, there was over a 1 °C difference in temperature between both slurries. This indicates that the QS slurry is drying quicker and the temperature of the slurry is recovering to room temperature. When the QS was dry to the touch, the AdBond Advantage was still drying as per the image within Figure 11.

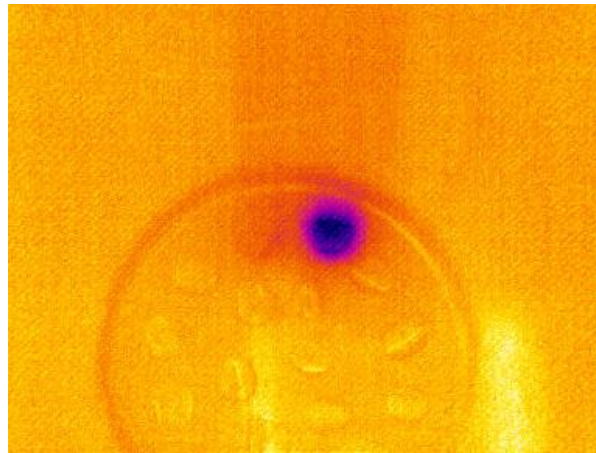


Figure 11 Thermal Image of Slurries after the QS slurry was dry

Dynamic Mechanical Analysis

The DMA results measure the modulus of the substrate and slurry during gelation. Care was taken to ensure the same volume of slurry was present for both samples. Figure 12 has the modulus for both AA and QS slurries. This is the first time we have been able to mechanically assess the gelation of a slurry. As can be seen below gelation occurs quite fast (in a matter of a minute or two).

Plot of Modulus against evaporation time for Adbond Advantage and Adbond Quikset coated on rubber substrate

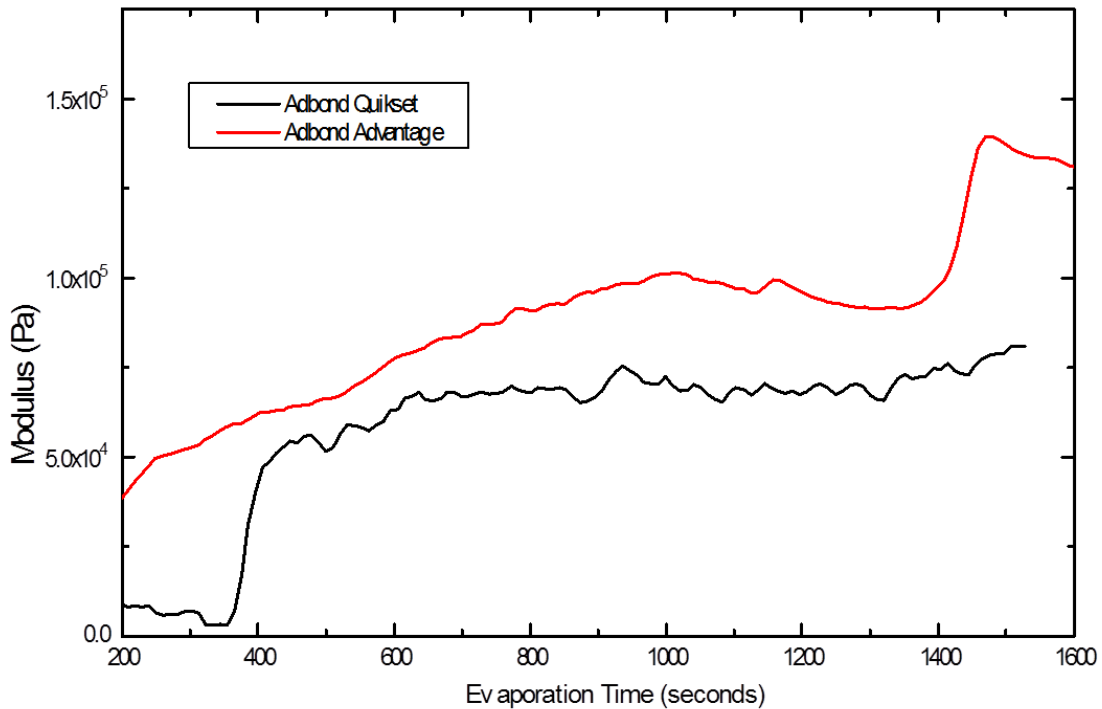


Figure 12 Plot of modulus vs. Evaporation time AA Slurry vs. QS slurry

The DMA results show the slow increase in modulus within the AA slurry sample as it slowly dries during testing. This then follows the sharp increase in modulus during gelation.

For QS, the gelation of the sol happens much quicker than with AA slurries due to the novel polymer present within the shell matrix. The onset of gelation occurs much quicker (71% quicker!) than the standard sol. Following gelation, there is still some increase in modulus as the slurry continues to dry.

Shell Trial

A shell trial was conducted within O'Fallon Casting to assess the feasibility of transferring from Ethyl Silicate (ES) shell system, to the QS shell system. O'Fallon Casting uses the ES system as an intermediate slurry for 3 to 5 layers between a single prime and backups. The ES system provides improved shell drying by using ammonia gelling. With this in mind, one of the main objective of the trial was to produce complex investment castings using QS but maintaining the same dry times as used for the ES system. In addition, the ease of knockout was critical to a successful trial. Improvements in one area of the plant cannot be successful if it reduces efficiency down the line. The final objective was to maintain similar dimensional results.

Initially, the slurry formulation was based on the current ES system. O'Fallon Casting uses mullite flour for the ES. To assist in maintaining dimensional results, it was also used in the trial slurry. The % solids and viscosity were kept constant, the % silica was controlled at 21%. Viscosity was measured using a #3 Zahn and silica was determined using density. The trial was conducted on multiple parts with a variety of complexity. Beginning the trial, parts were hand dipped; but as the trial progressed, robot dipping was utilized. In both cases, the same dry time and same environmental conditions (68-72F and 55-65% RH) as the ethyl silicate system were maintained. The samples were autoclaved and fired to 1450 °F for 1 hour, then pre-heated to part dependant mold temps. Parts were poured using A 356 aluminum, A 357 aluminum and aluminum matrix silicon carbide composites. Positive results occurred initially showing good surface finish without cracking or other shell related defects.

As parts became more complex, shell drying issues started to arise. O'Fallon casting started seeing excess metal in core passages and deep pockets (Figure 13).

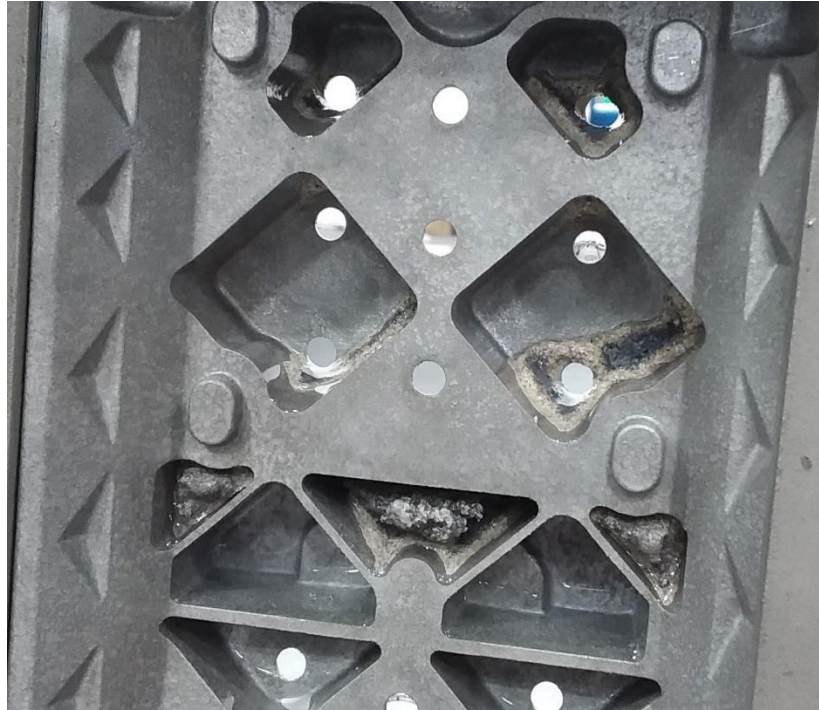


Figure 13. Image of excess metal in pockets

At this point, adjustments were made to both the slurry and the environmental conditions. The percent silica was changed to 23% in an attempt to reduce the amount of liquid in the system and also provide additional strength. To achieve this change, the amount of DI water was reduced by 40 lbs. and the binder was increased by 40 lbs. In addition, it was decided to try drying in a lower humidity environment more typical of a water-based shell system. Drying was performed between 35% and 45% relative humidity and increased air movement. Under these conditions, O'Fallon Casting successfully produced highly complex parts with similar dry times to the ES system.

Simultaneously, MOR shells and Perm balls were dipped to assess strength and permeability compared to the ethyl silica shell system. Figure 14 shows the MOR strength of the material.

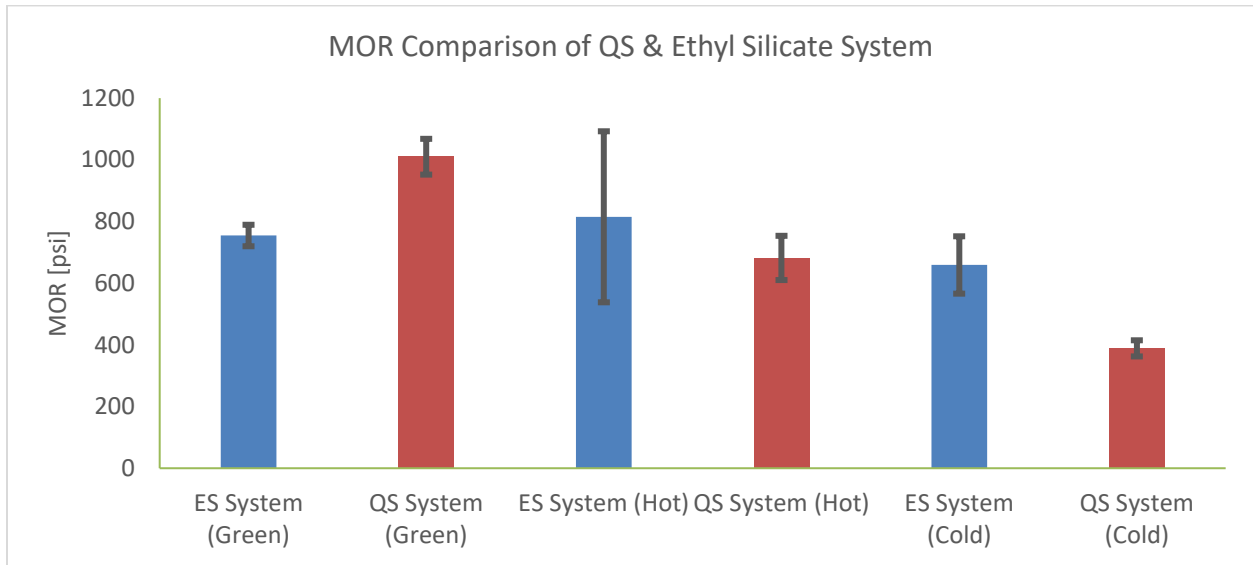


Figure 14. Chart of MOR strengths for both ES and QS systems

The QS shell system showed stronger by 34%. The strength was slightly lower for the hot strength by 16% although it must be stated the error is high for the ES shell system. Finally the QS shell system was lower due to the presence of the polymer, allowing for easier knockout of parts. The permeability tests showed almost double permeability in the QS system versus the ES system.

Four different parts were dimensionally inspected for the trial. Table 3 has summarizes the results for all 4 parts.

Table 3. Dimensional results of trial parts

Part #	Drawing Dimension with tolerance (inch)	ES Dimension (inch)	QS Dimension (inch)	Change from ES to QS (inch)
1	0.720 ± 0.020	0.7220	0.7228	0.0007
2	1.50 ± 0.015	1.4995	1.5034	0.0039
2	3.78 ± 0.020	3.7841	3.7785	-0.0056
3	13.31 ± 0.075	13.3434	13.3503	0.0068
4	1.590 ± 0.010	1.5950	1.5955	0.0005
4	0.630 ± .010	0.6279	0.6310	0.0031
4	1.380 ± .010	1.3742	1.3785	0.0043

All measurements for all parts fell within the dimensional tolerance allowed by the drawings and a few dimensions had almost no change between the 2 shell systems. However, several of the dimensions showed a significant difference between the ES and QS system. More dimensional testing is needed on a larger sample set to determine the exact impact of the QS system.

Conclusion

Remet has developed the use of DMA to assess the gelation of slurries. The increase in modulus of a slurry can be seen when an oscillating load is applied to an elastic rubber substrate with an applied slurry material.

QuikSet™ Polymer Concentrate can offer significant advances in shell room building with no requirement for capital investment. When compared to current slurries on the markets, QS can reduce dry times, occurrences of cracks and defects and improve permeability of the shell during casting. The QS polymer can ensure temperature and humidity deviations do not result in scrap and yield issues.

The trials conducted at O'Fallon Casting showed that QS can be used to replace ES, but will require conversion to a lower relative humidity with increased air movement. The presence of the polymer within the shell also works to reduce the cold strength allowing for better knock off. It has been found over the years that there have been some dimensional differences noted between ethyl silicate and water-based binder systems, even using the same refractory. Some speculate that the differences in sodium content of the binders plays a large part in this

References

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